

117 876 13 38.4 + 24 34 868 + 6.2 8615

66313

W 8025

6.11 + 0.86 + 0.70 16117 R

A058937
+ 2502640 1.5 0778 = 6.00

6 = 06 6.87 + 0.37 5.51

+1.1 591
0CW 4 + 048 - 213 66

-29 -64 -6 .010
-111 -82 -10 .007

+054 -53 -205 -54
+050 -210

+0039 -2065 AC +

+0039 -2045
+054 -2045 AC →
+053 -201 AB132 [1056 - 198] 4.0

+6.2

~~400355 ± 5.5~~ -213 ± 4.7
~~+0043~~ -202

26.022 1898.2 +24 34 19.86 18974

~~-151~~

~~25.~~ ~~841~~ ~~11.20~~
3 1.06

25.951

~~17~~

~~96~~

~~152~~

25.97

~~970~~

(31.1)

-

~~24~~

~~84~~

19 30.2

~~-24~~

~~564~~

~~24.69~~

~~29.3~~

~~31.9~~

~~-6.3~~

3

510

117874 1.3 30.7 +24 37 6.61+56 11422

1.6213

110355 515

+26

- 0.45 - 3.40 +

+056 - 2.08 Y > 1%

+058 - 2.04 A6612

+052 - 2.06

(4056 - 202)

117876.000*

13.000*

30.400*

24.000*

36.000*

0.056*

-0.198

4.000*

63.096

6.200

-0.775

-0.160

-79

-49.882

-0.585

0.054

14





900 080

117 880 13 30.8 - 18 15. - 44.6

9.02 + 0.105 = 10.15 (2)

Hoffmann & JP

-45.06

-0.62 - 142 Yale

$\frac{-0.13}{-0.38}$ - 112 Hohenbalk

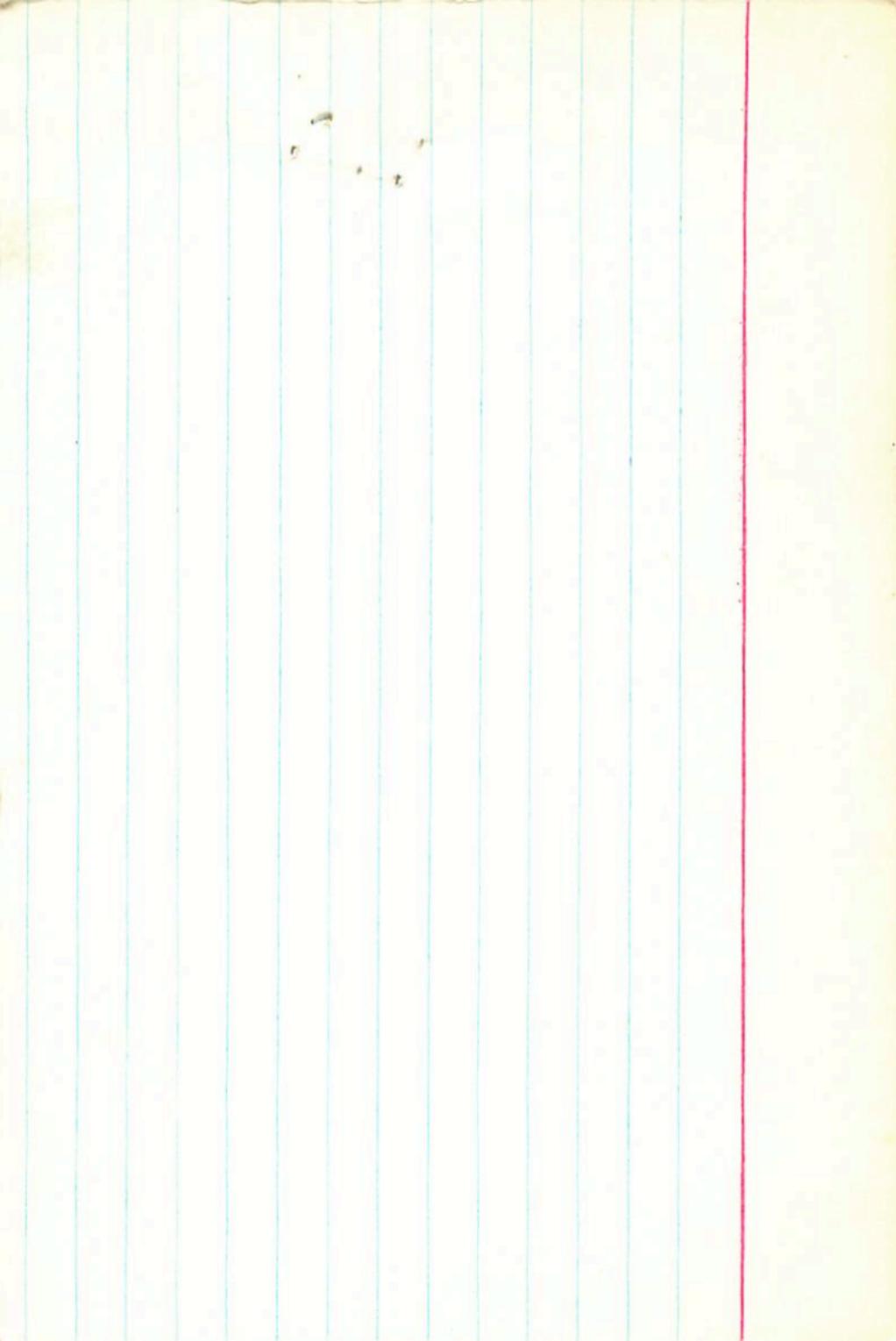
$\frac{-1.27}{-1.27}$

0.99

7.84

-85.66 / -140.33

4.80 1.10



Torsten Sondt

R5

(+0) 117 880

-17 038 830 1.3 30.6 -18 15 40.5 -15 R

$M_V = +1$ $v = 0$
 $V = -170$
 $w = -206$

9.08 +0.04 +0.06 Roman
-00 45 -065 -10

-00 45 -065 -10

44 -142 43 → 9.02 +0.10 +0.15 -061 +14 -135 +10 Y
M4 (W, V, R, G)
100 100 100 100 100 100

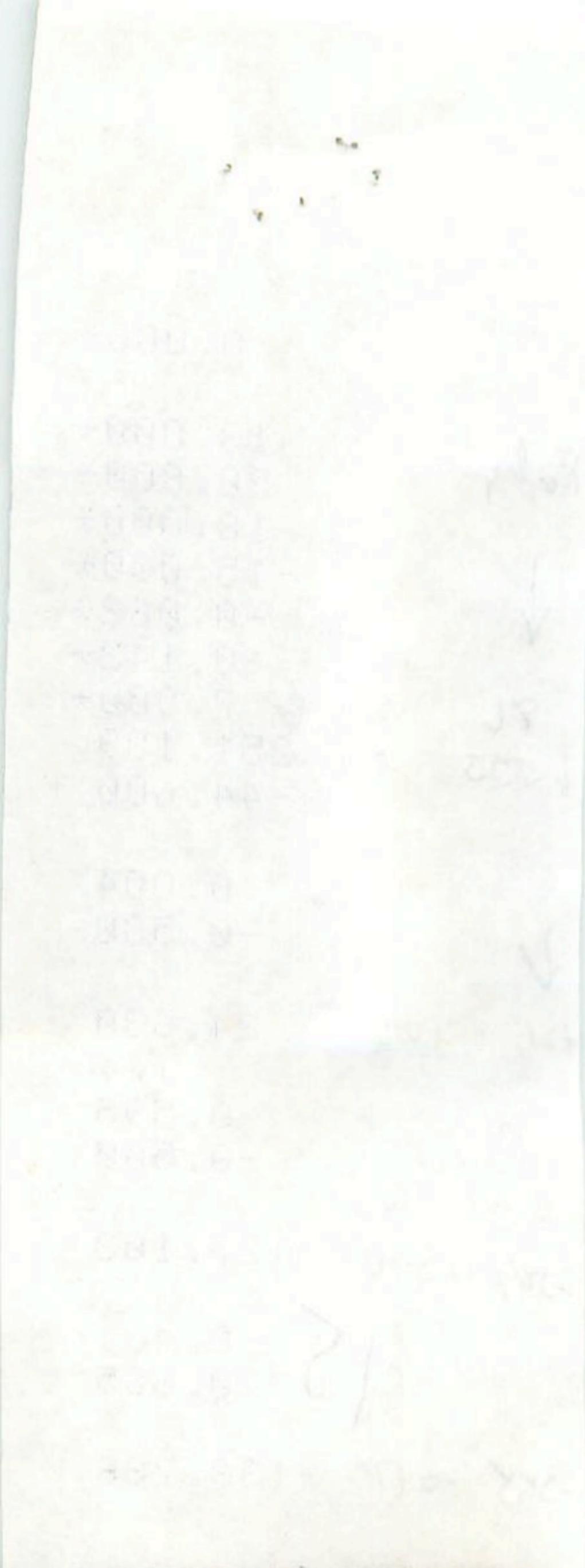
89966 -0027 -127

500
400 100
+23324 -22622 +0059 +3.0
-1748 -4164 -5964 -268.2
+01170 -4792 -4322 -216.1

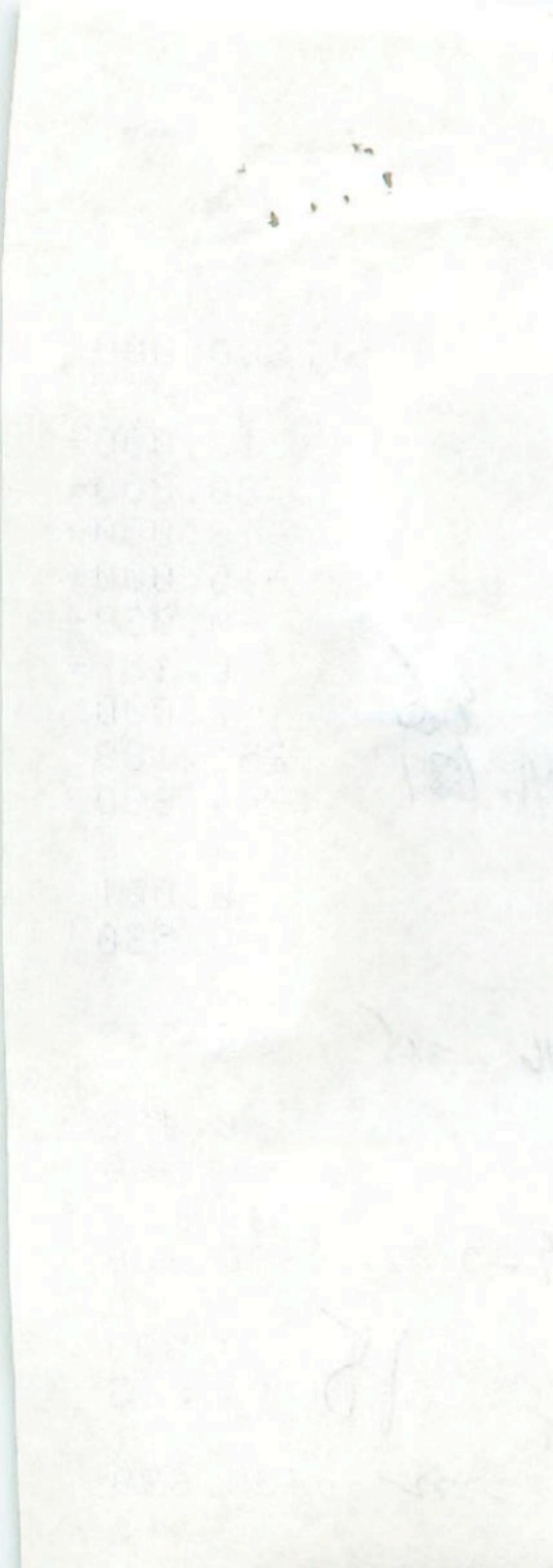
+26.7
-275.7
-247.2
-0.2
-23.9 +23.7 = -0.2
-193.2 +22.5 = -170.7
-3668 -156.9 -30.9 -190.8

459
7611
212

15



| | | |
|-------|------|------------|
| | | 0. 000 * |
| Rally | | 13. 000 * |
| | | -30. 800 * |
| | | -18. 000 * |
| | | -15. 000 * |
| | | -8. 062 * |
| | | -8. 142 * |
| 8.6 | 8.5 | 6.7. 000 * |
| 6523 | 501 | 251. 189 |
| | | -44. 600 |
| | | 0. 004 |
| | | -0. 530 |
| 426 | 426 | 24. 630 |
| | | 14. 9 |
| | | -0. 595 |
| | | -0. 500 |
| -289 | -276 | -127. 192 |
| | 15 | -0. 431 |
| | | 0. 685 |
| -255 | -247 | -138. 786 |



117880.0000

13.0000

30.0000

-18.0000

-15.0000

-0.0388

-0.1273

6217.0000

251.189

-44.600

-0.061

-0.530

16 -15 8.333

-0.482

-0.500

269.0 1903

-98.738

15 -0.399
0.685

272 -130.699

| | | |
|---|-----|--|
| OOC_2CH_3 | (s) | CH_3OH |
| $\text{OCS}(\text{CH}_3)_2$ | (s) | CH_3OH |
| OOCC_2CH_3 | (s) | CH_3OH |
| OOCC_2CO_2 | (s) | CH_3OH |
| $\text{OOC}_2\text{CH}_2\text{CH}_3$ | (s) | CH_3OH |
| $\text{CH}_3\text{C}_2\text{H}_5$ | (s) | $\text{CH}_3\text{CH}_2\text{CH}_2\text{OH}$ |
| $\text{OOC}_2\text{CH}_2\text{CH}_2\text{CH}_3$ | (s) | $\text{CH}_3\text{CH}_2\text{CH}_2\text{OH}$ |

| | | |
|----------------------------|-----|----------------------------|
| CH_3CO_2^- | (s) | CH_3CO_2^- |

| | | |
|----------------------------|-----|----------------------------|
| CH_3CO_2^- | (s) | CH_3CO_2^- |

| | | |
|----------------------------|-----|----------------------------|
| CH_3CO_2^- | (s) | CH_3CO_2^- |

| | | |
|-----------|---|----------|
| R.A. | : | 13.500 |
| DEC. | : | -18.250 |
| PM. R.A. | : | -86.000 |
| PM. DEC. | : | -140.000 |
| DISTANCE | : | 8.400 |
| MODULUS | : | 479 |
| RAD. VEL. | : | -44.600 |

| | | |
|--------|---|--------|
| q1 (U) | : | -0.781 |
| q2 (U) | : | 0.335 |
| q3 (U) | : | -0.527 |
| dU | : | 79.766 |
| U | : | 61.700 |

| | | |
|--------|---|----------|
| q1 (V) | : | 0.605 |
| q2 (V) | : | 0.619 |
| q3 (V) | : | -0.502 |
| dV | : | -644.537 |
| V | : | -286.113 |

| | | |
|--------|---|----------|
| q1 (W) | : | -0.158 |
| q2 (W) | : | 0.711 |
| q3 (W) | : | 0.686 |
| dW | : | -410.427 |
| W | : | -227.020 |

119055

13 82.0 -16 04 100 m

15.3675

8846.24

DM

1100,1000

110000-

-21

114

10

-101

106.1 ③

16

1980-1981
1981-1982
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2020-2021
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2079-2080
2080-2081
2081-2082
2082-2083
2083-2084
2084-2085
2085-2086
2086-2087
2087-2088
2088-2089
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2090-2091
2091-2092
2092-2093
2093-2094
2094-2095
2095-2096
2096-2097
2097-2098
2098-2099
2099-20100

R.A. : 13.550
DEC. : -16.050
R.A. : -21.000
DEC. : -16.000
STANCE : 1000
ODULUS : -101.100
LIEL :

* 1169 903 1930 066 666 1171 27

5114 13 33.1 +10 28

118264
19365

6.50 +10 6 +0.88 E
6.10 +0.355 (2) 15.2

574
526

8.64 +0.48 -0.02 E

9.9

5.22
10.5
11.3
11.8

5.21

[.338]

232
328
+0.12
+0.21

2628 0

A and B

+095 -060 46123

+076 -060 62 →

+091 -060 4
+063 -056 4
+32.7

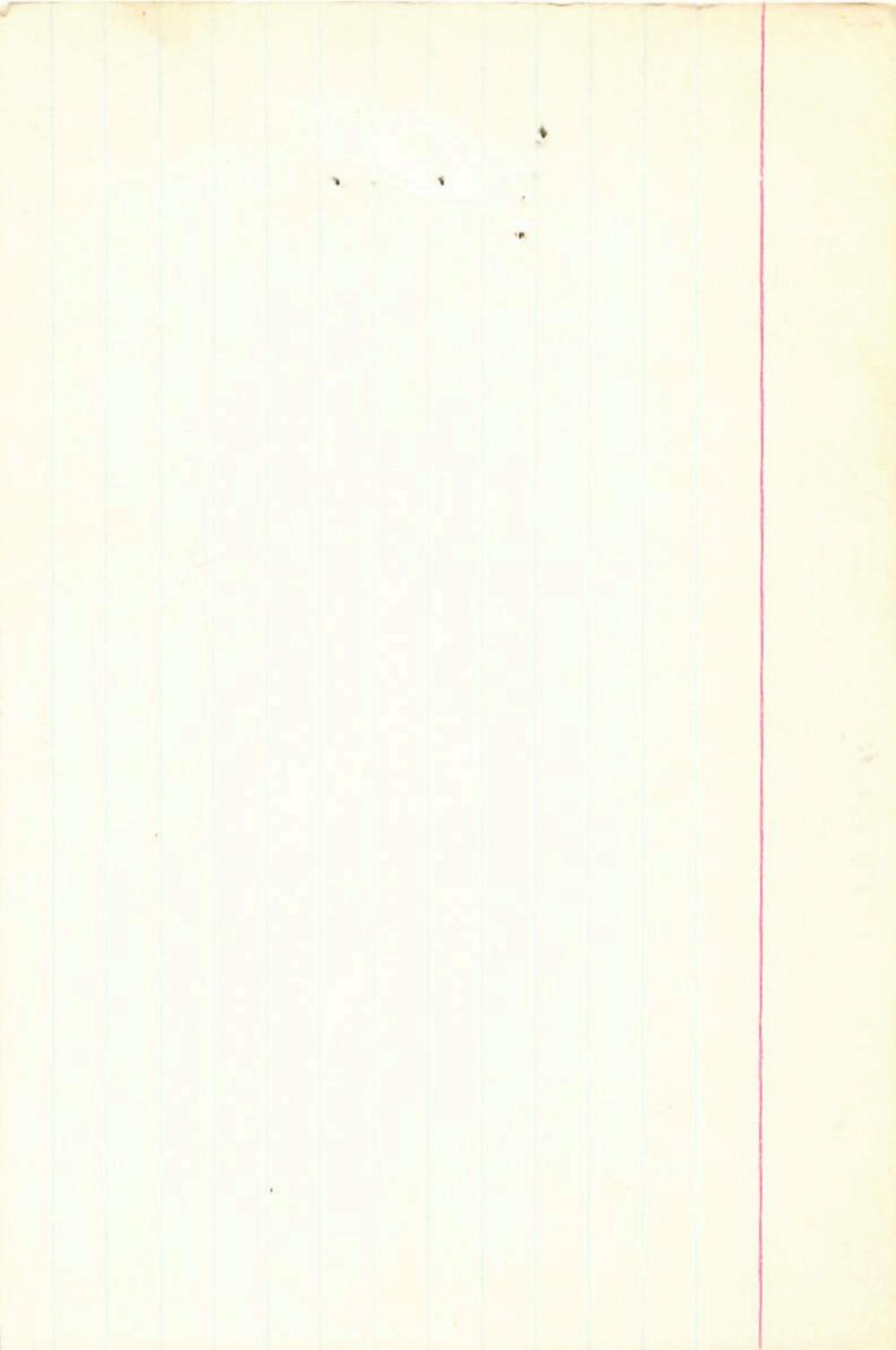
1013 054 carry

+093 -054

1171 040

1171

-84
858
347



$$\begin{array}{r}
 \text{Card II} \\
 118266 \\
 +0059 \\
 \hline
 +0059 \\
 -057 \\
 \hline
 00545
 \end{array}$$

$$4.143 \quad 1905.4 \quad +10 \quad 27 \quad 38.23 \quad 1600.3$$

$$\begin{array}{r}
 -223 \\
 -970 \\
 \hline
 3,970
 \end{array}$$

$$\begin{array}{r}
 +3.38 \\
 41.61 \\
 \hline
 41.61
 \end{array}$$

$$36.62$$

$$\begin{array}{r}
 1934.6 \\
 -40 \\
 \hline
 39.52
 \end{array}$$

$$1940.25$$

$$39.60$$

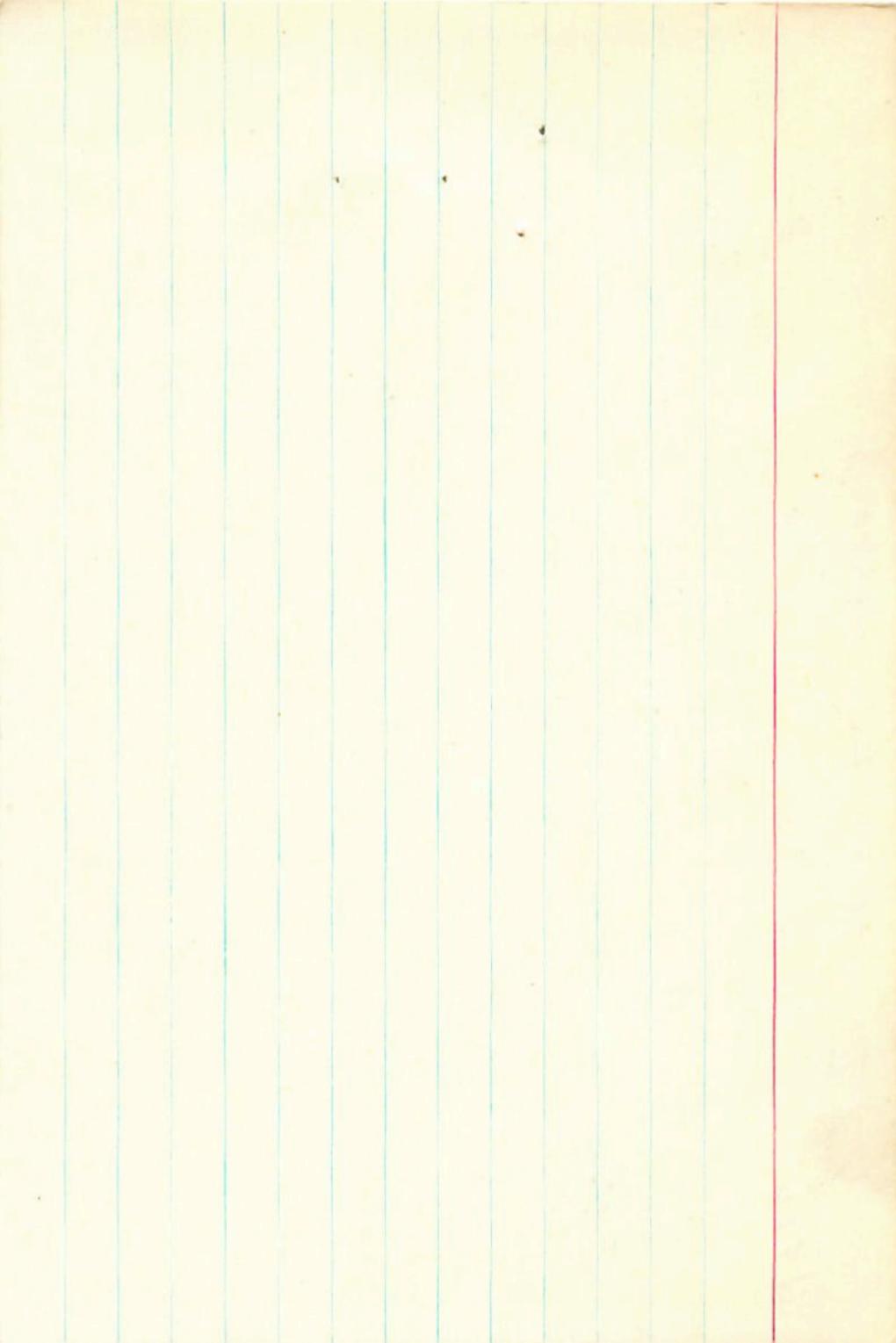
$$+4.85$$

$$37.4$$

$$\begin{array}{r}
 37.1 \\
 -2.11 \\
 \hline
 35.50
 \end{array}$$

$$\begin{array}{r}
 118 \\
 \overline{159} \\
 159 \\
 \hline
 0
 \end{array}$$

$$\begin{array}{r}
 32.0 \\
 +189 \\
 \hline
 273
 \end{array}$$



T₂

118266 11.6 13 33.1 +10 28 +32.7 +244}

6415365
w 8049
+10.02565

6.24

8.5 70"

118514
+1000566.99.

70"

6.47 +1.05 -0.015 2^{m 24}" (B) +0.71^{m 24} -0.4264
6.51 +1.07 +2.17 1^{m 24} +0.74 -0.666

0 8.91 +0.475 -0.015 2^{m 24}" (B) +0.88^{m 24} -0.4264
8.98 +0.50 +0.63 1^{m 24} 5.73

17.0

5.73

5.73

17.0

15.67/10⁵
10⁵

15.67/10⁵
10⁵

(-0.16) 0.0

K1, II, H

- 36 - 10 + 5 - 2025

$$\begin{array}{r} \text{A} \\ \boxed{4 + 11 = 15} \\ \hline 15 - 4 \\ \hline 11 \end{array}$$
$$\begin{array}{r} \boxed{14 + 01 = 15} \\ \hline 15 - 14 \\ \hline 1 \end{array}$$
$$\begin{array}{r} \boxed{6 + 5 + 7} \\ \hline 18 - 17 \\ \hline 1 \end{array}$$
$$\begin{array}{r} \boxed{17 - 62 - 35} \\ \hline 007 \end{array}$$

$$0249 - 005 - 0650120811 - 344 + 321 - 29 - 13$$
$$314 - 535 = 1314 / 535 = 2.45$$
$$535 - 314 = 221$$

| | | |
|-----------|---|----------|
| | | -4.127 |
| R.A. | : | 13.550 |
| R.A. | : | 14.000 |
| DEC. | : | 5.380 |
| DISTANCE | : | 119 |
| MAGNITUDE | : | 34.700 |
| VEL. | : | |
| q1 (U) | : | -0.775 |
| q2 (U) | : | 0.549 |
| q3 (U) | : | -0.312 |
| dU | : | -483.955 |
| U | : | -68.464 |
| q1 (V) | : | 0.608 |
| q2 (V) | : | 0.782 |
| q3 (V) | : | -0.135 |
| dV | : | 69.172 |
| V | : | 3.544 |
| q1 (M) | : | -0.169 |
| q2 (M) | : | 0.294 |
| q3 (M) | : | 0.941 |
| dM | : | -150.394 |
| M | : | 14.721 |

✓9

18439/40

116742 13 35.8 +89 26 062 -2144(3)

105888 / 8m = 2.4 3" (48)

m 8069 □ m = 3.66
mm.

431.8

18902663
1600 C 55" 9.6

0189 -143

-262-143

-225 -53 ≈ 16 1/2 Gc

C

-227-41 ≈ 16 1/4 Gc

-222
-162

7.78 40.67 +0.24 652
5 = -0.03
W (F4.1)

918 538 440

-365 -56

231683

27611 m(5)

-143
3.15
-340

-0194±3.2

-143±2.4

-406 -9141 635 -773 -222 -162 -242 -103 -552

-090 -042 203 094 -872 273 -18.6 +17 +5

-24 +43 -43 0215

416 -63 -4

51.634 / 832.5 + 39 26 1.49 / 1893.6

9.19

52.652

43.9
38.88

46.410

39.2

52.129

30.3

52.011

30.0

52.010

52.000

51.111

5

5.4
1930.2

5.32

5.02

5.220

5.220

5.220

5.220

5.220

5.220

5.220

5.220

5.220

5.220

3.4.2

2.7.9

000,000
824,98
000,000
000,000
000,000
000,000
000,000

AMERICAN
BANK & TRUST
COMPANY

R.A. : 13.600
DEC. : 39.450
R.A. : -368.000
DEC. : -143.000
PARCE : 3.150
MAGNUS : 43
MAGNUS : 21 000 350

664-12 13 37.24 +0 12.9

+44.0 h-1/m

11.48 +0.40 -0.22 2R .24 245° Wuf
G

④

6-14-12 13 37.5 40v 13 +
wef/1992

11.49 .40.38 -0.23 ~~50~~ 51

+438.5 ~~Plankage~~ (4)

11.2
L 0.95
21.5
V 9
4.75
1.62

-0.245 -0.115 Nichols (1) Partygo ~~L~~ 4.
-0.215 -0.105 Woy 51

Blue Slingshots

19

13. 0000

13. 0000

37. 5000

6. 0000

13. 0000

-0. 2400

-0. 1980

6. 0000

158. 489

438. 500

0. 625

-0. 419

-84. 914

-1. 000

-0. 260

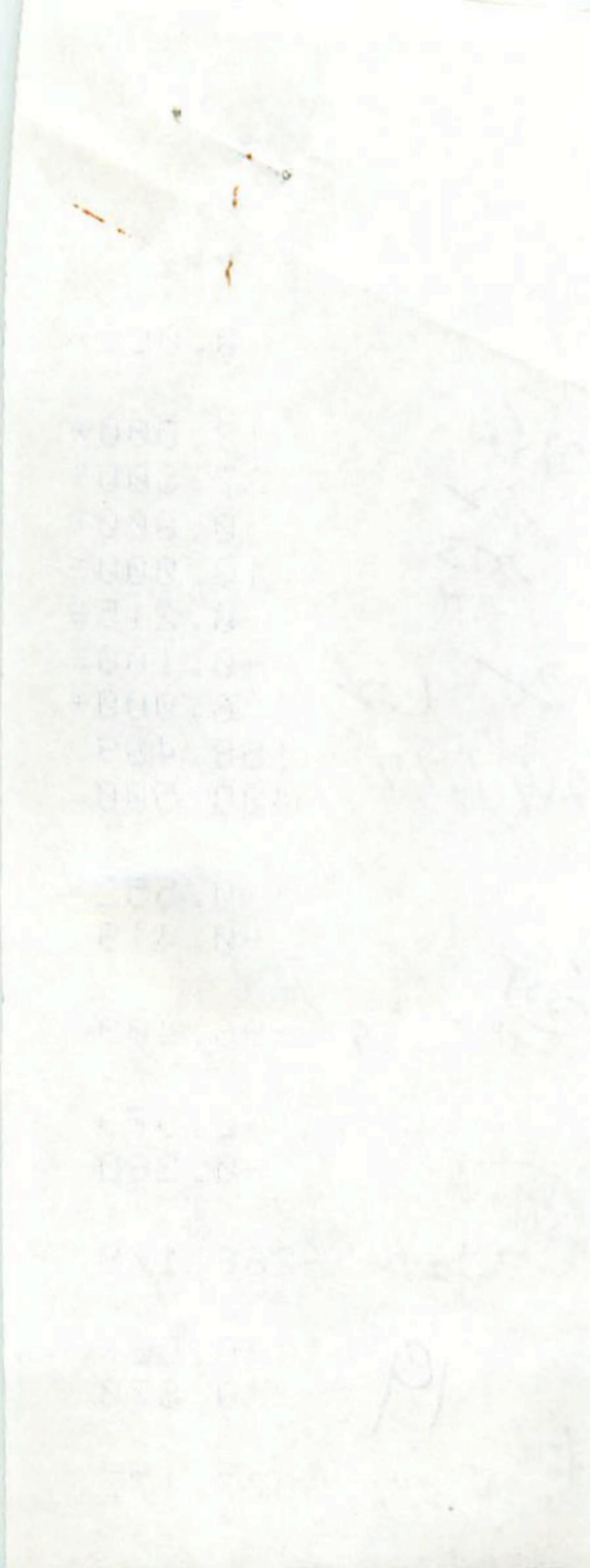
-285. 182

-0. 022

-0. 370

377. 933

19



| | | |
|-----|-------|--------------------|
| | | 0.000% |
| 272 | 1.4 | 13.000% |
| 275 | 1.4 | 37.500% |
| 32 | | 0.000% |
| 373 | | 13.000% |
| 437 | | -3.215% |
| 20 | 6.2 | -0.100% |
| 269 | 171.7 | 158.489 438.500 |
| -35 | | 0.552 -0.419 |
| -1 | -89 | -96.489 |
| 371 | | -0.979 -0.260 |
| 364 | 282 | -269.178 |
| 19 | | -0.027 0.870 |
| 377 | | 377.177 |

118781

13 32.5 + 3 2.7

+ 2.2705

66.261

064 - 225 /

145 P

X 272.0

136

+ 24

64

- 225 /

412

430

26

4.00

4.00

4.00

4.00

4.00

4.00

4.00

4.00

4.00

13.600
2.400
64.000

R.A. :
DEC. :

ADS 5002

119461 13 40.9 -4 01 2.0 8 124 +4.78
14553

8109 54.607 1904.9 -4 1 23.03 1900.9

124
727

9.528"
planned

41.37
21.66

36.869

427.59

17.777

-

28.6

23.27

6.723

6.723

6.723

6.723

6.723

22.23
4

22.23
4

22.23
4

22.23
4

22.23
4

6.99

1939.31

33.5

32.6

32.6

32.6

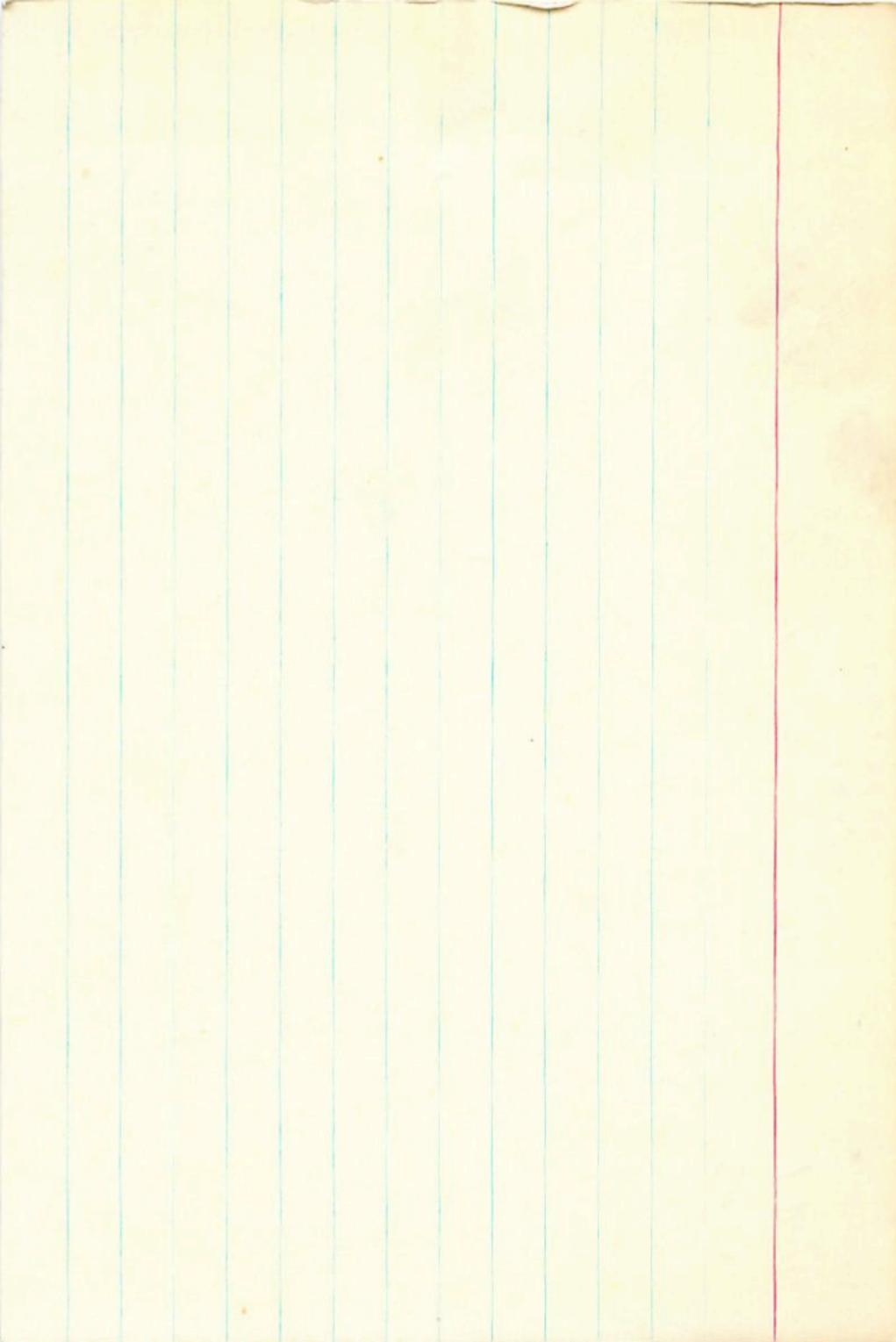
32.6

32.6

32.6

32.6

32.6



ADS 5000

179467

13 6639 -04 02 ~~462~~ 152 TII

$\bar{E} = +0.3$

7.10 +1.29 +1.21 3 E

6.55 +0.46 \uparrow acc.

+0.44

→ 6.49
10.83 / 10.12
3.5 3.5

6.53 6.326 [5.215]

+ $\frac{1.232}{0.18}$
3.33 + $\frac{1.232}{0.18}$

MV +3.50

Audhu

6.19
5.54
6.53
-0.8
10.10

②

[5.373]
 $\frac{3.15}{0.55}$

N.V = +0.3



1957 / 13 44-5 -50 04 115 430.4 a

6418627 1313 1045 182 5.45 +1.32 -6.45
 8134 09304 103 5.45 1.32
 7 3137 1612 103 +6.45
 -4908145

14R 5174 12 114 114 -0158 = 025 Oct -153 -030

2218.5 -0.026 +14 -60 +11
" 1.262-1079.117
153 0.36

15.0
- 35
17.67 1956.50

29.593
- 25
29.593

24.865
- 26
23.9
~~14.07~~
~~7.04~~
- 584

(37.1)

- 79
17.80
- 47
17.55
48.0
9596

(41.3)

17.05 1939.46

24.644 1910.9
- 22
22
+ 130
17.01
- 50 4 18.3
- 0157
- 0159 + 6.1
- 0157
- 0159 + 5.4

119871

6018627

13 44.5 -50 04 115 +3049

481341

+30.34 (3)

73137
-49 08164

642
+31.32 6ape

16.5 255 Gc
-153 -030
-143 +003 CP
-150 -017 6ct
-148 -010

5174 312 +11.5
5206 313 +14.5 +0.02 -2.75 5.5 9.5 -

+25 -57 +66 .0125

4510 410)

^s
+031 +.91

with

$$\Delta m_0 = .013$$

Z 1939.46

$$p=3$$

$$p_0 = 0.76$$

$$z_R = 0.387 \delta, z_{03} <$$

$$P_{.25m} = 4.93 S$$

+ 78
+ 75
+ 105
+ 126

12

$$\text{con. } M_S = -.017$$

$$\begin{array}{r} -440 -895 \\ -767 \quad 641 -148 -010 +30.4008 -23 -028 \\ -065 007 133 -007 -275 \quad 649 +19.5 -18 -9 \end{array}$$

$$\begin{array}{r} -40 +43 -25 \\ +25 -57 +16 \end{array} \quad 0125$$

2. 5

5

5

5

5

119971.0000

13.0000

44.5000

-50.0000

-4.0000

-0.1480

-0.0150

6.0000

158.489

30.400

65
199.5

642

0.531

-0.656

803 86

64.242

110

-0.457

-0.728

-113

-94.474

21

0.081

0.200

4117

+220

18.986

| | | | |
|-----------------------|---|---|---|
| OCX, O ⁻ | ? | ✓ | W |
| OCC, OC ⁻ | ? | ✓ | W |
| OOO, O ⁻ | ? | ✓ | W |
| OCS, CS ⁻ | ? | ✓ | W |
| OOC, CO ⁻ | ? | ✓ | W |
| <i>met</i> | ? | ✓ | W |
| OOP, OE ⁻ | ? | ✓ | W |
| <i>met</i> | ? | ✓ | W |
| <i>met</i> | ? | ✓ | W |
| EGN, O ⁻ | ? | ✓ | W |
| EGL, O ⁻ | ? | ✓ | W |
| Ncd, O ⁻ | ? | ✓ | W |
| ppf, pse | ? | ✓ | W |
| Ncb, O ⁻ | ? | ✓ | W |
| <i>met</i> | ? | ✓ | W |
| <i>met</i> | ? | ✓ | W |
| SSc, O ⁻ | ? | ✓ | W |
| SES, O ⁻ | ? | ✓ | W |
| NSN, O ⁻ | ? | ✓ | W |
| NCC, CNS ⁻ | ? | ✓ | W |
| Cdx, Cd ⁻ | ? | ✓ | W |
| <i>met</i> | ? | ✓ | W |
| <i>met</i> | ? | ✓ | W |
| GFS, O ⁻ | ? | ✓ | W |
| GGG, O ⁻ | ? | ✓ | W |
| GGG, O ⁻ | ? | ✓ | W |
| BIN, Bi ⁻ | ? | ✓ | W |
| OBP, O ⁻ | ? | ✓ | W |

| | | |
|-------|---|----------|
| R, A. | : | 13,750 |
| DEC. | : | -50,050 |
| R, A. | : | -141,000 |
| DEC. | : | -6,280 |
| ANGLE | : | 6,000 |
| JULUS | : | 158 |
| VEL. | : | 30,400 |
| 1 (U) | : | -0,753 |
| 2 (U) | : | -0,031 |
| 3 (U) | : | -0,657 |
| dU | : | 324,144 |
| U | : | 31,397 |
| 1 (V) | : | 0,622 |
| 2 (V) | : | 0,292 |
| 3 (V) | : | -0,727 |
| dV | : | -275,552 |
| V | : | -65,763 |
| 1 (W) | : | -0,215 |
| 2 (W) | : | 0,956 |
| 3 (W) | : | 0,200 |
| dW | : | 63,718 |
| W | : | 16,190 |