155102 17 06.1 +40 35 6.3 A8 -7.46

23128

9889

$-0036^{70}_{-030}{}^{63}$ N30

$-0034 \pm 1.6 - 033 \pm 1.6$ GC → N30

66.2 −0005 ±13.0 −094 ±13.0
−0022 −101

154810 17 06.2 −45 34 ~~8.14+48~~

23131 66.2 8.14+50+1.61 F8V −26.0±0.9 $C_2$(6)

cape

10.318 1902.6 −45 34 22.40 1902.4
024 4.47
342 17.93

−0014

Stop

10.230 −0023 −100 23.18 1955.50
−7 −9
223 23.27

−00185 −096
−0194

−021 −095

30 4.67

154810 17 06.2 -45 34 F8 V

8115 +50 -01 (1)

[M] 228

[C] 300

.324 .120 .365 2.646 (3) 5,10,4,6

85

17.100
-45.600
-30.000
-95.000
4.670
86
-26.000

85.50
66.07
18.83
65.76

-0.139
-0.279
-0.950
139.510
36.689

0.584
0.752
-0.306
-396.594
-26.110

-0.800
0.598
-0.059
-189.525
-14.748

-078 -1604 +14.8 Griffin

4C

154962 17 06.3 -3 49 G8 IV-V +12.7

FO 1231 +0.47 ? +14.8 (6) +13.8

GC 23133 6.35 +0.69 (1.84)

-0042 ±6.5 -162 ±6.3 -0042 -162 C+

16.514 1899.6 -0042 63.67 1899.7 -0041.5 -159

212 8.15 -062

.726 55.52 +13.8

-0040 -158 -060 -158 2.35

-060

+2

57.623 p.c 16.602 3.46 1933.32

18.968 -12 59.20 1933.57

16592 16.590 2.66 1.23

-15 2.05 +21

.577 2.61 1.02

-5

2.66

-058 -158

154962.000*

17.000*
6.300*
-3.000*
-43.000*
-0.058*
-0.158*
4.000*
63.096
14.800

-0.280
-0.895

-30.937

-0.733
0.273

-42.206

-0.143
0.353

-3.861

154962.000*

17.000*
6.300*
-3.000*
-49.000*
-0.060*
-0.158*
2.350*
29.512
13.800

-0.279
-0.895

-20.585

-0.739
0.273

-18.025

-0.136
0.353

0.875